

**TALAT Lecture 2301**

## **Design of Members**

### **Axial Force**

#### **Example 5.1 : Axial force resistance of square hollow section**

2 pages

Advanced Level

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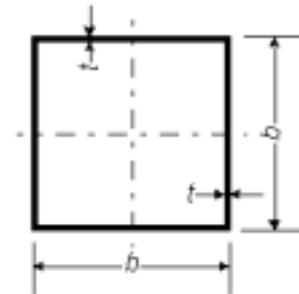
# Example 5.1. Axial force resistance of square hollow section

Width	$b := 70 \cdot \text{mm}$	$\text{MPa} \equiv 10^6 \cdot \text{Pa}$	$\text{kN} \equiv 1000 \cdot \text{newton}$
Thickness	$t := 1.9 \cdot \text{mm}$	$f_o := 200 \cdot \text{MPa}$	
Column length	$L := 1000 \cdot \text{mm}$	$E := 70000 \cdot \text{MPa}$	
		$\gamma_{M\bar{F}} = 1.0$	

## 5.4.3 Slenderness parameter

$$b_f := b - 2 \cdot t \quad b_f = 66.2 \cdot \text{mm}$$

$$\beta := \frac{b_f}{t} \quad \beta = 34.8$$



## 5.4.4 Element classification

$$\varepsilon := \sqrt{\frac{250 \cdot \text{MPa}}{f_o}} \quad \varepsilon = 1.118$$

Tab. 5.1

$\beta_{\bar{F}1} = 11 \cdot \varepsilon$	$\beta_{\bar{F}2} = 12.3$
$\beta_{\bar{F}2} = 16 \cdot \varepsilon$	$\beta_{\bar{F}3} = 17.9$
$\beta_{\bar{F}3} = 22 \cdot \varepsilon$	$\beta_{\bar{F}4} = 24.6$

$$\text{class} := \text{if}(\beta > \beta_{\bar{F}1}, \text{if}(\beta > \beta_{\bar{F}2}, \text{if}(\beta > \beta_{\bar{F}3}, 4, 3), 2), 1) \quad \text{class} = 4$$

## 5.4.5 Local buckling

5.4.5 (3) c)  
heat-treated  
unwelded

$$\rho_{\bar{c}} := \text{if}\left(\frac{\beta}{\varepsilon} \leq 22, 1.0, \frac{32}{\left(\frac{\beta}{\varepsilon}\right)} - \frac{220}{\left(\frac{\beta}{\varepsilon}\right)^2}\right) \quad \rho_{\bar{c}} = 0.8$$

$$t_{\text{eff}} := \text{if}(\text{class} \geq 4, t \cdot \rho_{\bar{c}}) \quad t_{\text{eff}} = 1.52 \cdot \text{mm}$$

$$A_{\text{eff}} := 4 \cdot (b - t) \cdot t_{\text{eff}} \quad A_{\text{eff}} = 414.2 \cdot \text{mm}^2$$

$$I := \frac{b^4}{12} - \frac{(b - 2 \cdot t)^4}{12} \quad I = 4.004 \cdot 10^5 \cdot \text{mm}^4$$

$$r := \sqrt{\frac{I}{A_{\text{eff}}}} \quad r = 31.1 \cdot \text{mm}$$

## 5.8.4 Flexural buckling

Table 5.7

$$K := 1 \quad l := K \cdot L$$

Table 5.5  
and 5.6

$$\alpha := 0.2 \quad \lambda_o := 0.1 \quad k_1 := 1 \quad k_2 := 1$$

See to the  
right

$$\lambda := \frac{l}{r} \cdot \frac{1}{\pi} \cdot \sqrt{\frac{f_o}{E}} \quad \lambda = 0.547$$

(5.33)

$$\phi := 0.5 \cdot \left[ 1 + \alpha \cdot (\lambda - \lambda_o) + \lambda^2 \right] \chi := \frac{1}{\phi + \sqrt{\phi^2 - \lambda^2}}$$

$$\phi = 0.694 \quad \chi = 0.891$$

5.8.3 (1)

$$N_{b,Rd} := \chi \cdot k_1 \cdot k_2 \cdot \frac{f_o}{\gamma_{M\bar{F}}} \cdot A_{\text{eff}}$$

$$N_{b,Rd} = 73.8 \cdot \text{kN}$$

According to 5.8.4.1 (1)

$$\lambda = \sqrt{\frac{A \cdot \eta \cdot f_o}{N_{cr}}}$$

Substitute

$$N_{cr} = \frac{\pi^2 \cdot E \cdot I}{l^2} \quad \eta = \frac{A_{\text{eff}}}{A} \quad r = \sqrt{\frac{I}{A_{\text{eff}}}}$$

Result

$$\lambda = \frac{l}{r} \cdot \frac{1}{\pi} \cdot \sqrt{\frac{f_o}{E}}$$

Note:  $\lambda$  with a bar cannot be written