

TALAT Lecture 2301

Design of Members

Axial Force

Example 5.4 : Axial force resistance of channel cross section

7 pages

Advanced Level

prepared by Torsten Höglund, Royal Institute of Technology, Stockholm

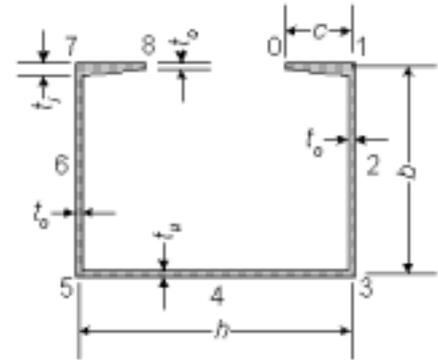
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Example 5.4. Axial force resistance of channel cross section

Width/depth $b := 80\text{-mm}$ $h := 100\text{-mm}$ $f_o := 300\text{-MPa}$ $kN \equiv 1000\text{-newton}$
 Inner thickness/outstand $t_i := 8\text{-mm}$ $c := 25\text{-mm}$ $E := 70000\text{-MPa}$ $G := \frac{E}{2.6}$ $MPa \equiv 10^6 \cdot Pa$
 Outer/bottom thickness $t_o := 3.5\text{-mm}$ $t_u := 4\text{-mm}$ $\gamma_{MF} := 1.0$
 Length $L := 1200\text{-mm}$

$i := 0..8$ $k := 1..3$
 Nodes no., co-ordinates, thickness
 $tl_i := t_o$ $th_i := t_o$ $y_k := 0.5 \cdot h$ $z_i := b$
 $th_1 := t_i$ $tl_8 := t_i$ $y_{k+4} := -0.5 \cdot h$ $z_{k+2} := 0\text{-mm}$
 $th_4 := t_u$ $tl_4 := t_u$ $y_4 := 0\text{-mm}$ $z_2 := 0.5 \cdot z_1$
 $th_5 := th_4$ $tl_5 := tl_4$ $y_0 := 0.5 \cdot h - c$ $z_6 := 0.5 \cdot z_1$
 $y_8 := -y_0$ $z_1 := z_1 - 0.5 \cdot (t_i - t_o)$
 $z_7 := z_1$



$i =$	$\frac{y_i}{mm} =$	$\frac{z_i}{mm} =$	$\frac{tl_i}{mm} =$	$\frac{th_i}{mm} =$
0	25	80	3.5	3.5
1	50	77.75	3.5	8
2	50	40	3.5	3.5
3	50	0	3.5	3.5
4	0	0	4	4
5	-50	0	4	4
6	-50	40	3.5	3.5
7	-50	77.75	3.5	3.5
8	-25	80	8	3.5

Nodes $i := 1..rows(y) - 1$

Cross-section constants, varying thickness

Sectorial co-ordinates

$$\omega_0 := 0 \cdot mm^2$$

$$\omega_i := y_{i-1} \cdot z_i - y_i \cdot z_{i-1}$$

$$\omega_i := \omega_{i-1} + \omega_i$$

Thicknesses to simplify expressions

$$Dt_i := th_i - tl_i \quad tl_i := tl_i + \frac{Dt_i}{2}$$

$$t2_i := \frac{tl_i}{2} + \frac{Dt_i}{3}$$

$$t3_i := \frac{tl_i}{3} + \frac{Dt_i}{4}$$

Length of elements

$$l_i := \sqrt{(y_i - y_{i-1})^2 + (z_i - z_{i-1})^2}$$

Area

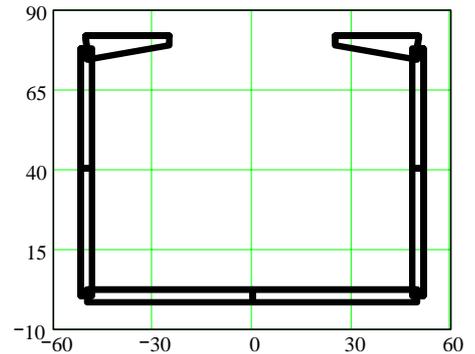
$$A := \sum_{i=1}^{rows(y)-1} \frac{tl_i + th_i}{2} \cdot l_i$$

$$A = 1.233 \cdot 10^3 \cdot mm^2$$

First moments of area

$$S_z := \sum_{i=1}^{rows(y)-1} [y_{i-1} \cdot tl_i + (y_i - y_{i-1}) \cdot t2_i] \cdot l_i$$

$$S_z = -8.47 \cdot 10^{-13} \cdot mm^3$$



$$S_y := \sum_{i=1}^{\text{rows}(y)-1} [z_{i-1} \cdot t l_i + (z_i - z_{i-1}) \cdot t 2_i] \cdot l_i \quad S_y = 4.388 \cdot 10^4 \cdot \text{mm}^3$$

$$S_\omega := \sum_{i=1}^{\text{rows}(y)-1} [\omega_{i-1} \cdot t l_i + (\omega_i - \omega_{i-1}) \cdot t 2_i] \cdot l_i \quad S_\omega = -7.328 \cdot 10^6 \cdot \text{mm}^4$$

Second moments of area

$$I_z := \sum_{i=1}^{\text{rows}(y)-1} [(y_{i-1})^2 \cdot t l_i + 2 \cdot y_{i-1} \cdot (y_i - y_{i-1}) \cdot t 2_i + (y_i - y_{i-1})^2 \cdot t 3_i] \cdot l_i$$

$$I_y := \sum_{i=1}^{\text{rows}(y)-1} [(z_{i-1})^2 \cdot t l_i + 2 \cdot z_{i-1} \cdot (z_i - z_{i-1}) \cdot t 2_i + (z_i - z_{i-1})^2 \cdot t 3_i] \cdot l_i$$

Mixed

$$I_\omega := \sum_{i=1}^{\text{rows}(y)-1} [(\omega_{i-1})^2 \cdot t l_i + 2 \cdot \omega_{i-1} \cdot (\omega_i - \omega_{i-1}) \cdot t 2_i + (\omega_i - \omega_{i-1})^2 \cdot t 3_i] \cdot l_i$$

$$I_{yz} := \sum_{i=1}^{\text{rows}(y)-1} [(y_{i-1}) \cdot (z_{i-1}) \cdot t l_i + [y_{i-1} \cdot (z_i - z_{i-1}) + z_{i-1} \cdot (y_i - y_{i-1})] \cdot t 2_i + (y_i - y_{i-1}) \cdot (z_i - z_{i-1}) \cdot t 3_i] \cdot l_i$$

$$I_{y\omega} := \sum_{i=1}^{\text{rows}(y)-1} [(y_{i-1}) \cdot (\omega_{i-1}) \cdot t l_i + [y_{i-1} \cdot (\omega_i - \omega_{i-1}) + \omega_{i-1} \cdot (y_i - y_{i-1})] \cdot t 2_i + (y_i - y_{i-1}) \cdot (\omega_i - \omega_{i-1}) \cdot t 3_i] \cdot l_i$$

$$I_{z\omega} := \sum_{i=1}^{\text{rows}(y)-1} [(z_{i-1}) \cdot (\omega_{i-1}) \cdot t l_i + [z_{i-1} \cdot (\omega_i - \omega_{i-1}) + \omega_{i-1} \cdot (z_i - z_{i-1})] \cdot t 2_i + (z_i - z_{i-1}) \cdot (\omega_i - \omega_{i-1}) \cdot t 3_i] \cdot l_i$$

Influence of thickness

$$I_a := \overline{\left[(t l_i + t h_i) \cdot \left[(t l_i)^2 + (t h_i)^2 \right] \cdot \frac{l_i}{48} \right]} \quad I_{yz} := I_{yz} + \sum_{i=1}^{\text{rows}(y)-1} \frac{I_a \cdot (y_i - y_{i-1}) \cdot (z_i - z_{i-1})}{(l_i)^2}$$

$$I_z := I_z + \sum_{i=1}^{\text{rows}(y)-1} \frac{I_a \cdot (z_i - z_{i-1})^2}{(l_i)^2} \quad I_y := I_y + \sum_{i=1}^{\text{rows}(y)-1} \frac{I_a \cdot (y_i - y_{i-1})^2}{(l_i)^2}$$

$$I_t := \sum_{i=1}^{\text{rows}(y)-1} (t l_i + t h_i) \cdot \left[(t l_i)^2 + (t h_i)^2 \right] \cdot \frac{l_i}{12} \cdot 1.05 \quad I_t = 8.425 \cdot 10^3 \cdot \text{mm}^4$$

$$z_{gc} := \frac{S_y}{A} \quad z_{gc} = 35.593 \cdot \text{mm} \quad I_y := I_y - A \cdot z_{gc}^2 \quad I_y = 1.325 \cdot 10^6 \cdot \text{mm}^4$$

$$y_{gc} := \frac{S_z}{A} \quad y_{gc} = 0 \cdot \text{mm} \quad I_z := I_z - A \cdot y_{gc}^2 \quad I_z = 2.151 \cdot 10^6 \cdot \text{mm}^4$$

$$I_{yz} := I_{yz} - \frac{S_y \cdot S_z}{A} \quad I_{yz} = -1.816 \cdot 10^{-10} \cdot \text{mm}^4 \quad I_{y\omega} := I_{y\omega} - \frac{S_z \cdot S_\omega}{A} \quad I_{y\omega} = 1.057 \cdot 10^8 \cdot \text{mm}^5$$

$$I_\omega := I_\omega - \frac{S_\omega^2}{A} \quad I_\omega = 9.438 \cdot 10^9 \cdot \text{mm}^6 \quad I_{z\omega} := I_{z\omega} - \frac{S_y \cdot S_\omega}{A} \quad I_{z\omega} = 5.294 \cdot 10^{-8} \cdot \text{mm}^5$$

Shear centre

$$y_{sc} := \frac{I_{z\omega} \cdot I_z - I_{y\omega} \cdot I_{yz}}{I_y \cdot I_z - I_{yz}^2} \quad z_{sc} := \frac{-I_{y\omega} \cdot I_y + I_{z\omega} \cdot I_{yz}}{I_y \cdot I_z - I_{yz}^2}$$

$$y_{sc} = 4.668 \cdot 10^{-14} \cdot mm$$

$$z_{sc} = -49.159 \cdot mm$$

Warping constant

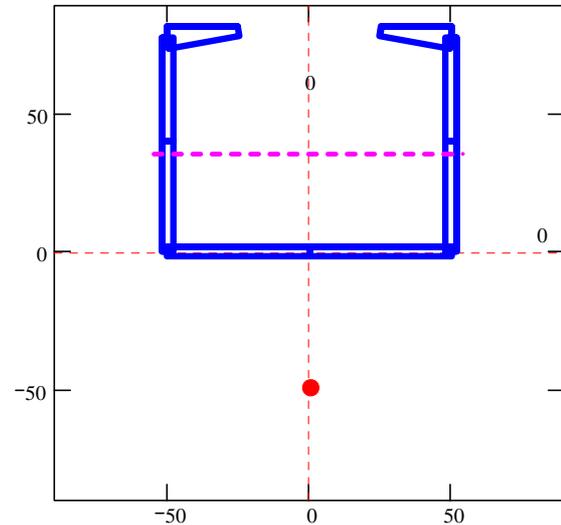
$$I_w := I_\omega + z_{sc} \cdot I_{y\omega} - y_{sc} \cdot I_{z\omega}$$

$$I_w = 4.24 \cdot 10^9 \cdot mm^6$$

Polar radius gyration

$$i_p := \sqrt{\frac{I_y + I_z}{A} + (y_{sc} - y_{gc})^2 + (z_{sc} - z_{gc})^2}$$

$$i_p = 100 \cdot mm$$



Buckling of stiffened flanges

5.4.5 Local buckling, internal elements $i := 3, 5..7$

$$\varepsilon := \sqrt{\frac{250 \cdot MPa}{f_o}} \quad \varepsilon = 0.913$$

$$\beta_i := \sqrt{\left[(y_i - y_{i-2})^2 + (z_i - z_{i-2})^2 \cdot \frac{2}{t_{l_{i-1}} + t_{h_i}} \right]}$$

5.4.5 (3) c
heat-treated
unwelded

$$\rho_{\xi} := \text{if} \left[\frac{\beta_i}{\varepsilon} \leq 22, 1.0, \frac{32}{\left(\frac{\beta_i}{\varepsilon}\right)^2} - \frac{220}{\left(\frac{\beta_i}{\varepsilon}\right)^2} \right]$$

$$t_{efl_i} := \rho_{\xi} \cdot t_{l_i} \quad t_{efh_i} := \rho_{\xi} \cdot t_{h_i}$$

$$t_{efl_{i-1}} := \rho_{\xi} \cdot t_{l_i} \quad t_{efh_{i-1}} := \rho_{\xi} \cdot t_{h_i}$$

$$\beta_i = \rho_{\xi} \cdot \frac{t_{efl_i}}{mm} = \frac{t_{efh_i}}{mm}$$

22.214	0.943	3.302	3.302
25	0.875	3.501	3.501
22.214	0.943	3.302	3.302

5.4.5 Local buckling, outstand elements $i := 1, 8..8$

$$t_{fic_i} := \text{if} \left[t_{l_i} > t_{h_i}, \left[(t_{l_i})^3 \cdot t_{h_i} \right]^{\frac{1}{4}}, \left[(t_{h_i})^3 \cdot t_{l_i} \right]^{\frac{1}{4}} \right]$$

$$\beta_i := \sqrt{\left[(y_i - y_{i-1})^2 + (z_i - z_{i-1})^2 \cdot \frac{1}{t_{fic_i}} \right]}$$

5.4.5 (3) c
heat-treated
unwelded

$$\rho_{\xi} := \text{if} \left[\frac{\beta_i}{\varepsilon} \leq 6, 1.0, \frac{10}{\left(\frac{\beta_i}{\varepsilon}\right)} - \frac{24}{\left(\frac{\beta_i}{\varepsilon}\right)^2} \right] \quad t_{efl_i} := \rho_{\xi} \cdot t_i \quad t_{efh_i} := \rho_{\xi} \cdot t_i \cdot \beta_i$$

$$\beta_i = \rho_{\xi} = \frac{t_{fic_i}}{\text{mm}} = \frac{t_{efl_i}}{\text{mm}} = \frac{t_{efh_i}}{\text{mm}} =$$

3.858	1	6.506	3.5	8
3.858	1	6.506	8	3.5

Reference: Pekoz, T., Flanges of nonuniform thickness.
Aluminium Design Workshop, Cornell University Oct. 1997

Buckling of edge stiffener

$i := 1..2$

$z_2 = 40 \cdot \text{mm}$

Effective
area

$$t1_i := t_{efl_i} + \frac{t_{efh_i} - t_{efl_i}}{2} \quad t2_i := \frac{t_{efl_i}}{2} + \frac{t_{efh_i} - t_{efl_i}}{3}$$

Length of
elements

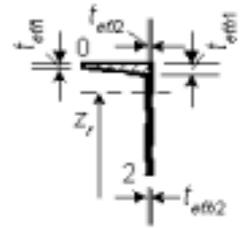
$$l_i := \sqrt{(y_i - y_{i-1})^2 + (z_i - z_{i-1})^2}$$

Area

$$A_r := \sum_{i=1}^2 \frac{t_{efl_i} + t_{efh_i}}{2} \cdot l_i \quad A_r = 269 \cdot \text{mm}^2$$

Centre of
gravity

$$z_r := \sum_{i=1}^2 [z_{i-1} \cdot t1_i + (z_i - z_{i-1}) \cdot t2_i] \cdot l_i \cdot \frac{1}{A_r} \quad z_r = 69.528 \cdot \text{mm}$$



Second moment
of area

$i := 1..2$

$z_2 := z_1 - 15 \cdot (t2_2 + th_2) \cdot 0.5 \quad z_6 := z_2$

$z_2 = 25.25 \cdot \text{mm}$

$$Dt_i := th_i - t_i \quad t1_i := t_i + \frac{Dt_i}{2} \quad t2_i := \frac{t_i}{2} + \frac{Dt_i}{3} \quad t3_i := \frac{t_i}{3} + \frac{Dt_i}{4}$$

Length of
elements

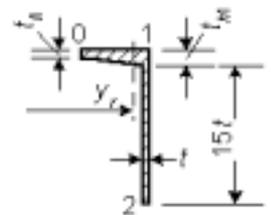
$$l_i := \sqrt{(y_i - y_{i-1})^2 + (z_i - z_{i-1})^2}$$

Area

$$A_{rI} := \sum_{i=1}^2 \frac{t1_i + th_i}{2} \cdot l_i \quad A_{rI} = 328.1 \cdot \text{mm}^2$$

Centre of
gravity

$$y_r := \sum_{i=1}^2 [y_{i-1} \cdot t1_i + (y_i - y_{i-1}) \cdot t2_i] \cdot l_i \cdot \frac{1}{A_{rI}} \quad y_r = 45.218 \cdot \text{mm}$$



Second moments of area

$$I_r := \sum_{i=1}^2 \left[(y_{i-1})^2 \cdot t l_i + 2 \cdot y_{i-1} \cdot (y_i - y_{i-1}) \cdot t z_i + (y_i - y_{i-1})^2 \cdot t z_i^2 \right] \cdot l_i - y_r^2 \cdot A_r$$

$$z_2 := z_1 \cdot 0.5$$

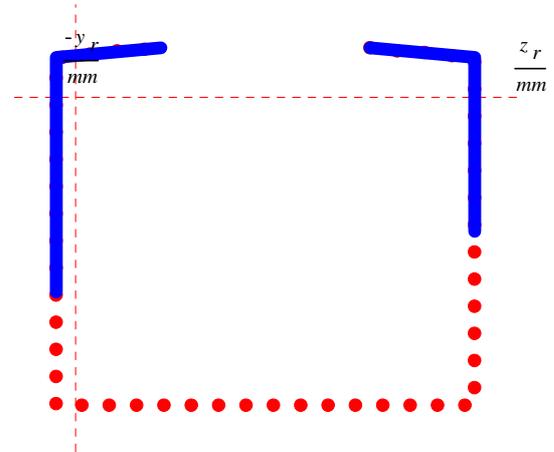
$$z_6 := z_2$$

$$k := 6..8 \quad i := 0..2 \quad j := 0..8$$

$$I_r = 1.668 \cdot 10^4 \cdot \text{mm}^4$$

Left: Cross section for second moment of area I_r based on t

Right: Effective cross section area A_r based on t_{ef}



$$s_I := y_3 - y_5$$

$$b_I := z_r$$

$$N_{r.cr} := 1.05 \cdot E \cdot \sqrt{\frac{I_r \cdot (th_3)^3}{b_I^3 \cdot \left[1 + \frac{1.5 \cdot s_I \cdot (th_4)^3}{b_I \cdot (th_3)^3} \right]}}$$

$$b_I = 69.528 \cdot \text{mm}$$

$$s_I = 100 \cdot \text{mm}$$

$$N_{r.cr} = 52.195 \cdot \text{kN}$$

Table 5.5 and 5.8

$$\alpha := 0.2$$

$$\lambda_I := 0.6$$

$$\lambda_c := \sqrt{\frac{f_o \cdot A_r}{N_{r.cr}}}$$

$$\lambda_{\bar{c}} = 1.243$$

(5.37)

$$\phi := 0.5 \cdot \left[1 + \alpha \cdot (\lambda_c - \lambda_I) + \lambda_c^2 \right] \chi_{\bar{c}} := \frac{1}{\phi + \sqrt{\phi^2 - \lambda_c^2}} \chi_r := \text{if}(\chi_r > 1, 1, \chi_r)$$

$$\phi = 1.337$$

$$\chi_{\bar{c}} = 0.547$$

$$i := 1..2 \quad t_{efl_i} := \chi_{\bar{c}} \cdot t_{efl_i} \quad t_{efh_i} := \chi_{\bar{c}} \cdot t_{efh_i}$$

$$i := 7..8 \quad t_{efl_i} := \chi_{\bar{c}} \cdot t_{efl_i} \quad t_{efh_i} := \chi_{\bar{c}} \cdot t_{efh_i}$$

$$i := 1..8$$

Length of elements

$$l_i := \sqrt{(y_i - y_{i-1})^2 + (z_i - z_{i-1})^2}$$

Area

$$A_{eff} := \sum_{i=1}^8 \frac{t_{efl_i} + t_{efh_i}}{2} \cdot l_i \quad A_{eff} = 904.9 \cdot \text{mm}^2$$

$$\frac{t_{efl_i}}{\text{mm}} = \frac{t_{efh_i}}{\text{mm}} = \frac{l_i}{\text{mm}} =$$

1.913	4.372	25.101
1.805	1.805	38.875
3.302	3.302	38.875
3.501	3.501	50
3.501	3.501	50
3.302	3.302	38.875
1.805	1.805	38.875
4.372	1.913	25.101

Axial force resistance, flexural-torsional buckling

Buckling length $l := L$

$$l = 1200 \cdot \text{mm}$$

Reference buckling loads

$$N_{Ey} := \frac{\pi^2 \cdot E \cdot I_y}{l^2} \quad N_{Ez} := \frac{\pi^2 \cdot E \cdot I_z}{l^2} \quad N_T := \left(G \cdot I_t + \frac{\pi^2 \cdot E \cdot I \omega}{l^2} \right) \cdot \frac{1}{i_p^2}$$

$$N_{Ey} = 635.91 \cdot kN \quad N_{Ez} = 1.03 \cdot 10^3 \cdot kN \quad N_T = 475.37 \cdot kN \quad \text{Guess: } N := 0.2 \cdot N_{Ez}$$

Given

$$(N_{Ey} - N) \cdot (N_{Ez} - N) \cdot (N_T - N) \cdot i_p^2 - (z_{sc} - z_{gc})^2 \cdot N^2 \cdot (N_{Ey} - N) - (y_{sc} - y_{gc})^2 \cdot N^2 \cdot (N_{Ez} - N) = 0$$

Solution

$$N_{cr} := \text{minerr}(N) \quad N_{cr} = 348.11 \cdot kN$$

General cross-section

Table 5.5 and 5.8

$$\alpha := 0.35 \quad \lambda_I := 0.4 \quad k_2 := 1$$

$$(\lambda_c = \lambda_{bar}) \quad \lambda_c := \sqrt{\frac{f_o \cdot A_{eff}}{N_{cr}}} \quad \lambda_{\bar{c}} = 0.883$$

(5.37)

$$\phi := 0.5 \cdot \left[1 + \alpha \cdot (\lambda_c - \lambda_I) + \lambda_c^2 \right] \chi := \frac{1}{\phi + \sqrt{\phi^2 - \lambda_c^2}} \quad \phi = 0.974 \quad \chi = 0.721$$

Table 5.5

$$\psi := \frac{|\min(z - z_{gc})| - |\max(z - z_{gc})|}{|\min(z - z_{gc})| + |\max(z - z_{gc})|} \quad \min(z - z_{gc}) = -35.6 \cdot mm \quad \psi = -0.11$$

$$\max(z - z_{gc}) = 44.4 \cdot mm$$

Table 5.5

$$k_I := 1 - 2.4 \cdot \psi^2 \cdot \frac{\lambda_c^2}{(1 + \lambda_c^2) \cdot (1 + \lambda_I^2)^2} \quad k_I = 0.996$$

5.8.3 (1)

$$N_{b.Rd} := \chi \cdot k_I \cdot k_2 \cdot \frac{f_o}{\gamma_{MI}} \cdot A \quad N_{b.Rd} = 265.8 \cdot kN$$